## Appendix B

## ARMSTRONG COTTAM

## DEVELOPMENT

## TRAFFIC IMPACT STUDY



RC SPENCER ASSOCIATES inc.
Consulting Engineers
Windsor: 800 University Ave. W. - Windsor ON N9A 5R9 Leamington: 18 Talbot St. W. - Leamington ON N8H 1M4
Chatham-Kent: 138 King St. W. Unit 102 - Chatham ON N7M 1E3

## INTRODUCTION AND BACKGROUND

A residential development has been proposed for lands in the Community of Cottam on the north side of Country Road 34 east of County Road 27. The proposed development is situated in the Town of Kingsville, in the County of Essex. The area is illustrated on Figure 1.

The proposed site plan consists of 32 single family detached housing units, as illustrated on Figure 2. The proposed residential development is situated behind existing residential units, with one access point into and out of the development onto County Road 34.

It has been requested that the study take account of the undeveloped lands to the north of this development. Figure 3 illustrates the location of these presently undeveloped lands. It is assumed that these lands will eventually be developed to consist of 47 single family detached housing units. Realistically, all of the future developed lands will access County Road 27 and County Road 34 by Whitewood Road and the Belleview Drive extension respectively. Greenwood Avenue will not likely be used by any of the trips generated by the proposed developments.

County Road 34 and County Road 27 are arterial roads with a County of Essex County Road status. Within the study area of this report, the intersection of these two roadways is stopcontrolled with County Road 34 having the right-of-way.

The purpose of this study is to examine the traffic implications of the proposed developments on traffic operations in the area, particularly on the intersection of County Road 34 and County Road 27.

## EXISTING CONDITIONS

Turning movement counts were obtained on Wednesday, December 20, 2017, for the intersection of County Road 34 at Countr Road 27, as provided in Appendix A. These counts were analyzed in the Synchro 10 program, which calculates various parameters of intersection performance such as Level of Service (LOS) and Intersection Capacity Utilization (ICU).

The results of the analysis show that the intersection of County Road 34 at Countr Road 27 is performing very well in the PM peak time period, with an overall LOS A during the peak hour. The ICU is $39.5 \%$ in the PM peak hour.

## TRIP GENERATION AND DISTRIBUTION

The proposed development contains one type of land use. ITE Land Use Code 210 (Single-Family Detached Housing) is the most appropriate code for this use. The respective land use code can be found in Appendix B. Trips under this land use code are typical for the expected use of the proposed residential area. It provides generation rates of 0.99 trips per unit in the PM peak hour with $63 \%$ in and $37 \%$ out. The AM peak was not considered because the trip generation rate is much lower, with 0.74 trips generated per unit. Likewise, the same land use code also applies to the adjacent undeveloped land. Again, it provides generation rates of 0.99 trips per unit in the PM peak hour with $63 \%$ in and $37 \%$ out.

The basis of the trip distribution assumptions is the turning movement count data obtained on Wednesday, December 20, 2017 for this location. The ratio of westbound to eastbound movements at the intersection of County Road 34 and County Road 27 formed the basis of the distribution to and from the proposed site. The ratios of turning movements by approach were the basis of distributing the site generated trips at the identified intersection. At full build-out, all trips to and from the north are expected to use the Whitewood Road access onto County Road 27, while all trips to and from the south, east, and west are expected to use the proposed Belleview Drive extension onto County Road 34.

When these estimates of trip distribution are applied to the trip generation estimates as previously summarized, the turning movements illustrated on Figure 4 - Site Generated Traffic result. These numbers have been added to existing and future volumes in order to analyze the traffic impact of the proposed developments.

## CAPACITY AND LEVEL OF SERVICE ANALYSIS

Figure 5A illustrates the existing traffic volumes for the PM peak hour for the intersection of County Road 34 and County Road 27. Subsequently, Figure 5B illustrates the anticipated traffic volumes for the PM peak hour when site generated traffic is added to the existing traffic at the aforementioned intersection.

In order to accommodate future growth, existing volumes have been increased across the board by $10 \%$, which would be approximately equal to growth in the range of $1 \%$ per year compounded over 10 years. Site generated traffic was added to this future estimate, and the results are presented in Figure 5C.

The data summarized in Figures 5A to 5C were used in the Synchro analysis of intersection performance. The results are summarized in tabular form in Figure 6 - Intersection Performance Summaries and in detailed form in Appendix C - Detailed Synchro Results. Each Synchro report found in Appendix C corresponds to an aforementioned figure reference.

From the summary table in Figure 6, for this intersection, it is observed that the addition of site traffic to existing traffic conditions does not change the LOS A rating, nor does it change for the future and site generated traffic conditions. In the future growth scenario, the ICU for the County Road 34 and County Road 27 intersection is $44.5 \%$. Therefore, no traffic operations concerns stemming from the development of the proposed site can be anticipated, as the proposed development does not add a significant amount of vehicular activity to on-street traffic conditions in either the immediate or future peak hour scenarios.

## SITE-SPECIFIC TRAFFIC SAFETY CONSIDERATIONS

Regarding the safety of site-specific traffic operations, it is noted that the access to the proposed residential development is about 90 m southeast of the Clark Street at County Road 34 intersection. To determine if existing geometries could pose a traffic safety hazard, the Transportation Association of Canada's Geometric Design Guide for Canadian Roads was used as a reference. From the manual, for a design speed of $50 \mathrm{~km} / \mathrm{h}$, intersection sight distance of 104 m is considered sufficient for safe operations at the site access. The corresponding calculations for intersection sight distance can be found in Appendix D.

Based on existing geometries, there is no obstruction to sight lines, and both Clark Street and the proposed Belleview Drive extension to County Road 34 will be able to operate safely and independently of each other. Therefore, daylight corners are not necessary at the proposed Belleview Drive access to County Road 34.

Additionally, it should be noted that, given the anticipated low turning volumes at Whitewood Road and Greenwood Avenue at County Road 27, there is no concern regarding safe traffic operations at these two intersections. Both intersections will continue to operate very similarly to status quo.

## SUMMARY AND CONCLUSIONS

A residential development has been proposed for lands just east of the intersection of County Road 34 and County Road 27, consisting of 32 single family detached housing units. Future trip generation of the presently undeveloped lands to the north of this proposed development were also considered.

Using recently obtained turning movement counts and the best available trip generation and distribution data, an analysis was completed to measure the operational impact of the development on conditions at the stop-controlled intersection of County Road 34 and County Road 27. The results indicate that the intersection will continue to operate at a very good level of service under full site development, even with future traffic growth of $10 \%$ above existing.

Since intersection sight distance of 104 m is considered sufficient for safe operations at the site access and there is no obstruction to sight lines, both Clark Street and the proposed Belleview Drive extension to County Road 34 will be able to operate safely and independently of each other. Therefore, daylight corners are not necessary at the proposed Belleview Drive access to County Road 34. Also, both Whitewood Road and Greenwood Avenue at County Road 27 will continue to operate very similarly to status quo with no concern regarding safe traffic operations.

All of which is respectfully submitted,

## RC Spencer Associates Inc.



John D. Torfiemire, M.A.Sc., P. Eng.
Manager, Leamington Office









| SPENCER ASSOCIATES inc. <br> Consulting Engineers <br> Windsor: 800 University Ave. W. - Windsor ON N9A 5R9 <br> Leamington: 18 Talbot St. W. - Leamington ON N8H IM4 <br> Chatham-Kent: 138 King St. W. Unit 102 - Chatham ON N7M IE3 | CESIGN | A.D.B. | ARMSTRONG COTTAM DEVELOPMENT | $\begin{array}{\|l\|} \hline \text { PROUECT NO. } \\ 17-657 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: |
|  | DRAWN | A.D.B. | $\begin{gathered} \text { C.R. } 27 / \underset{\text { EXISTING TRAFFIC }}{\text { C.R. } 34} \end{gathered}$ | FIGURE No. 5A |
|  | CHECKED J.T. |  |  |  |
| NIIM | DATE | JANUARY 2017 |  |  |
| Ontario | SCALE | N.T.S. |  | OF 6 |






## Intersection Performance Summary

|  |  | County Road 27 @ <br> County Road 34 |  |
| :---: | :---: | :---: | :---: |
|  | AM | LOS | ICU |
|  | PM | A | N/A |
| Existing \& Site | AM | N/A | N/A |
| Generated | PM | A | $41.4 \%$ |
| Future \& Site | AM | N/A | N/A |
| Generated | PM | A | $44.5 \%$ |


| Abrc spencer associatesinc. Consulting EngineersWindsor: 800 University Ave. W. - Windsor ON N9A 5R9 Leamington: 18 Talbot St. W.- Leamington ON N8H 1M4Chatham-Kent: 138 King St. W. Unit 102 . Chatham ON N7M 1E3 | [DESIGN A.O.B. <br> CHECKED  <br> J.T.  | ARMSTRONG COTTAM DEVELOPMENT | $\begin{gathered} \text { PROUECT NO. } \\ 17-657 \end{gathered}$ |
| :---: | :---: | :---: | :---: |
|  | DRAWN A. A.B. | INTERSECTION PERFORMANCE SUMMARY | FIGURE No. |
|  | CHECCED J.T. |  | 6 |
| VIIM | DAIE Janvary 2017 <br> SCALE n.t.s. |  | OF 6 |

## Appendix A

## TRAFFIC COUNTS

RC SPENCER ASSOCIATES inc.
Consulting Engineers
Windsor: 800 University Ave. W. - Windsor ON N9A 5R9
Leamington: 18 Talbot St. W. - Leamington ON N8H 1M4
Chatham-Kent: 138 King St. W. Unit 102 - Chatham ON N7M 1E3

Date: December 20, 2017
Counted by: Robert Botham
Weather Conditions: Clear
Intersection: CR34 at CR27

Groups Printed- P. Veh. - Trucks - Buses

|  | County Road 34 E N/B |  |  |  | County Road 34 W S/B |  |  |  | County Road 27 W E/B |  |  |  | County Road 27 E W/B |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 04:30 PM | 8 | 29 | 2 | 39 | 7 | 22 | 5 | 34 | 1 | 13 | 10 | 24 | 5 | 15 | 11 | 31 | 128 |
| 04:45 PM | 12 | 23 | 4 | 39 | 6 | 28 | 8 | 42 | 6 | 11 | 11 | 28 | 4 | 15 | 12 | 31 | 140 |
| Total | 20 | 52 | 6 | 78 | 13 | 50 | 13 | 76 | 7 | 24 | 21 | 52 | 9 | 30 | 23 | 62 | 268 |
| 05:00 PM | 15 | 22 | 2 | 39 | 7 | 29 | 6 | 42 | 5 | 11 | 5 | 21 | 1 | 13 | 9 | 23 | 125 |
| 05:15 PM | 8 | 24 | 5 | 37 | 9 | 28 | 2 | 39 | 3 | 13 | 6 | 22 | 3 | 10 | 14 | 27 | 125 |
| 05:30 PM | 17 | 27 | 3 | 47 | 12 | 29 | 1 | 42 | 3 | 9 | 8 | 20 | 1 | 14 | 16 | 31 | 140 |
| 05:45 PM | 7 | 19 | 1 | 27 | 9 | 22 | 7 | 38 | 0 | 10 | 7 | 17 | 5 | 6 | 12 | 23 | 105 |
| Total | 47 | 92 | 11 | 150 | 37 | 108 | 16 | 161 | 11 | 43 | 26 | 80 | 10 | 43 | 51 | 104 | 495 |
| Grand Total | 67 | 144 | 17 | 228 | 50 | 158 | 29 | 237 | 18 | 67 | 47 | 132 | 19 | 73 | 74 | 166 | 763 |
| Apprch \% | 29.4 | 63.2 | 7.5 |  | 21.1 | 66.7 | 12.2 |  | 13.6 | 50.8 | 35.6 |  | 11.4 | 44 | 44.6 |  |  |
| Total \% | 8.8 | 18.9 | 2.2 | 29.9 | 6.6 | 20.7 | 3.8 | 31.1 | 2.4 | 8.8 | 6.2 | 17.3 | 2.5 | 9.6 | 9.7 | 21.8 |  |
| P. Veh. | 65 | 143 | 16 | 224 | 50 | 158 | 29 | 237 | 17 | 64 | 47 | 128 | 19 | 73 | 73 | 165 | 754 |
| \% P. Veh. | 97 | 99.3 | 94.1 | 98.2 | 100 | 100 | 100 | 100 | 94.4 | 95.5 | 100 | 97 | 100 | 100 | 98.6 | 99.4 | 98.8 |
| Trucks | 2 | 1 | 1 | 4 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 4 | 0 | 0 | 0 | 0 | 8 |
| \% Trucks | 3 | 0.7 | 5.9 | 1.8 | 0 | 0 | 0 | 0 | 5.6 | 4.5 | 0 | 3 | 0 | 0 | 0 | 0 | 1 |
| Buses | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| \% Buses | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1.4 | 0.6 | 0.1 |

## RC SPENCER ASSOCIATES inc.

Consulting Engineers
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Leamington: 18 Talbot St. W. - Leamington ON N8H 1M4 Chatham-Kent: 138 King St. W. Unit 102 - Chatham ON N7M 1E3


RC SPENCER ASSOCIATES inc.
Consulting Engineers
Windsor: 800 University Ave. W. - Windsor ON N9A 5R9
Leamington: 18 Talbot St. W.- Leamington ON N8H 1M4 Chatham-Kent: 138 King St. W. Unit 102 - Chatham ON N7M 1E3

|  | County Road 34 E N/B |  |  |  | County Road 34 W S/B |  |  |  | County Road 27 W E/B |  |  |  | County Road 27 E W/B |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 04:30 PM to 05:45 PM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 04:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:45 PM | 12 | 23 | 4 | 39 | 6 | 28 | 8 | 42 | 6 | 11 | 11 | 28 | 4 | 15 | 12 | 31 | 140 |
| 05:00 PM | 15 | 22 | 2 | 39 | 7 | 29 | 6 | 42 | 5 | 11 | 5 | 21 | 1 | 13 | 9 | 23 | 125 |
| 05:15 PM | 8 | 24 | 5 | 37 | 9 | 28 | 2 | 39 | 3 | 13 | 6 | 22 | 3 | 10 | 14 | 27 | 125 |
| 05:30 PM | 17 | 27 | 3 | 47 | 12 | 29 | 1 | 42 | 3 | 9 | 8 | 20 | 1 | 14 | 16 | 31 | 140 |
| Total Volume | 52 | 96 | 14 | 162 | 34 | 114 | 17 | 165 | 17 | 44 | 30 | 91 | 9 | 52 | 51 | 112 | 530 |
| \% App. Total | 32.1 | 59.3 | 8.6 |  | 20.6 | 69.1 | 10.3 |  | 18.7 | 48.4 | 33 |  | 8 | 46.4 | 45.5 |  |  |
| PHF | . 765 | . 889 | . 700 | . 862 | . 708 | . 983 | . 531 | . 982 | . 708 | . 846 | . 682 | . 813 | . 563 | . 867 | . 797 | . 903 | . 946 |

## Appendix B

## ITE TRIP GENERATION MANUAL - $10^{\text {TH }}$ EDITION

 REFERENCES
## Single-Family Detached Housing

(210)

Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m.<br>Setting/Location: General Urban/Suburban<br>Number of Studies: 173<br>Avg. Num. of Dwelling Units: 219<br>Directional Distribution: 25\% entering, 75\% exiting

Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.74 | $0.33-2.27$ | 0.27 |

## Data Plot and Equation



## Single-Family Detached Housing

(210)

Vehicle Trip Ends vs: Dwelling Units<br>On a: Weekday,<br>Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.<br>Setting/Location: General Urban/Suburban<br>Number of Studies: 190<br>Avg. Num. of Dwelling Units: 242<br>Directional Distribution: 63\% entering, 37\% exiting

Vehicle Trip Generation per Dwelling Unit

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.99 | $0.44-2.98$ | 0.31 |

## Data Plot and Equation



## Appendix C

## DETAILED SYNCHRO RESULTS

|  | $\cdots$ | $\pm$ | 2 | n | k | ¢ | \% | $\nearrow$ | Pa | 4 | $\grave{ }$ | * |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | $\dagger$ |  |  | $\dagger$ |  |  | \$ |  |  | $\uparrow$ |  |
| Traffic Volume (vph) | 29 | 158 | 50 | 17 | 144 | 67 | 47 | 67 | 18 | 74 | 73 | 19 |
| Future Volume (vph) | 29 | 158 | 50 | 17 | 144 | 67 | 47 | 67 | 18 | 74 | 73 | 19 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.972 |  |  | 0.960 |  |  | 0.981 |  |  | 0.984 |  |
| Flt Protected |  | 0.994 |  |  | 0.996 |  |  | 0.983 |  |  | 0.978 |  |
| Satd. Flow (prot) | 0 | 1800 | 0 | 0 | 1781 | 0 | 0 | 1796 | 0 | 0 | 1793 | 0 |
| Flt Permitted |  | 0.994 |  |  | 0.996 |  |  | 0.983 |  |  | 0.978 |  |
| Satd. Flow (perm) | 0 | 1800 | 0 | 0 | 1781 | 0 | 0 | 1796 | 0 | 0 | 1793 | 0 |
| Link Speed (kh) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance ( m ) |  | 223.2 |  |  | 281.3 |  |  | 234.2 |  |  | 285.7 |  |
| Travel Time (s) |  | 16.1 |  |  | 20.3 |  |  | 16.9 |  |  | 20.6 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 32 | 172 | 54 | 18 | 157 | 73 | 51 | 73 | 20 | 80 | 79 | 21 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 258 | 0 | 0 | 248 | 0 | 0 | 144 | 0 | 0 | 180 | 0 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 39.5\% ICU Level of Service A |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |


|  | $\cdots$ | $\pm$ | $\lambda$ | n | k | $\checkmark$ | \% | $\nearrow$ | T | 4 | $\backslash$ | K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Volume (vph) | 31 | 176 | 50 | 18 | 154 | 67 | 47 | 71 | 20 | 74 | 75 | 20 |
| Future Volume (vph) | 31 | 176 | 50 | 18 | 154 | 67 | 47 | 71 | 20 | 74 | 75 | 20 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.974 |  |  | 0.962 |  |  | 0.980 |  |  | 0.984 |  |
| Flt Protected |  | 0.994 |  |  | 0.996 |  |  | 0.983 |  |  | 0.979 |  |
| Satd. Flow (prot) | 0 | 1803 | 0 | 0 | 1785 | 0 | 0 | 1794 | 0 | 0 | 1794 | 0 |
| Flt Permitted |  | 0.994 |  |  | 0.996 |  |  | 0.983 |  |  | 0.979 |  |
| Satd. Flow (perm) | 0 | 1803 | 0 | 0 | 1785 | 0 | 0 | 1794 | 0 | 0 | 1794 | 0 |
| Link Speed (kh) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance ( m ) |  | 223.2 |  |  | 281.3 |  |  | 234.2 |  |  | 285.7 |  |
| Travel Time (s) |  | 16.1 |  |  | 20.3 |  |  | 16.9 |  |  | 20.6 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 34 | 191 | 54 | 20 | 167 | 73 | 51 | 77 | 22 | 80 | 82 | 22 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 279 | 0 | 0 | 260 | 0 | 0 | 150 | 0 | 0 | 184 | 0 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |  |  |  |  |  |
| $\frac{\text { Intersection Capacity Utilization 41.4\% }}{\text { Analysis Period (min) } 15}$ ICU Level of Service A |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |


|  | $\cdots$ | * | $\lambda$ | $\cdots$ | $k$ | ¢ | \% | $\nearrow$ | T | 4 | $\grave{ }$ | * |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | \$ |  |
| Traffic Volume (vph) | 34 | 192 | 55 | 20 | 168 | 74 | 52 | 78 | 22 | 81 | 82 | 22 |
| Future Volume (vph) | 34 | 192 | 55 | 20 | 168 | 74 | 52 | 78 | 22 | 81 | 82 | 22 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.974 |  |  | 0.962 |  |  | 0.980 |  |  | 0.984 |  |
| Flt Protected |  | 0.994 |  |  | 0.996 |  |  | 0.983 |  |  | 0.979 |  |
| Satd. Flow (prot) | 0 | 1803 | 0 | 0 | 1785 | 0 | 0 | 1794 | 0 | 0 | 1794 | 0 |
| Flt Permitted |  | 0.994 |  |  | 0.996 |  |  | 0.983 |  |  | 0.979 |  |
| Satd. Flow (perm) | 0 | 1803 | 0 | 0 | 1785 | 0 | 0 | 1794 | 0 | 0 | 1794 | 0 |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 50 |  |  | 50 |  |
| Link Distance (m) |  | 223.2 |  |  | 281.3 |  |  | 234.2 |  |  | 285.7 |  |
| Travel Time (s) |  | 16.1 |  |  | 20.3 |  |  | 16.9 |  |  | 20.6 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 37 | 209 | 60 | 22 | 183 | 80 | 57 | 85 | 24 | 88 | 89 | 24 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 306 | 0 | 0 | 285 | 0 | 0 | 166 | 0 | 0 | 201 | 0 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 44.5\% $\begin{aligned} & \text { Analysis Period (min) 15 }\end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

## Appendix D

## SIGHT LINE ANALYSIS CONSIDERATIONS

## Design Intersection Sight Distance (TAC Geometric Design Guide for Canadian Roads)

## Design Speed: Posted 50km/h

Table 9.9.3: Time Gap for Case B1, Left Turn from Stop

| Design Vehicle | Time Gap $\left(\boldsymbol{t}_{\boldsymbol{g}}\right)(\boldsymbol{s})$ at <br> Design Speed of Major Road |
| :--- | :---: |
| Passenger car | 7.5 |
| Single-unit truck | 9.5 |
| Combination truck (WB 19 and WB 20) | 11.5 |
| Longer truck | To be established by road authority |

Intersection Stopping Distance (ISD) $=0.278 \mathrm{~V}_{\text {major }} \mathrm{t}_{\mathrm{g}}$
Where:
ISD = intersection sight distance (m)
(length of the leg of sight triangle along the major road)
$\mathrm{V}_{\text {major }}=$ design speed of the major road (km/h)
$\mathrm{t}_{\mathrm{g}}=$ time gap for minor road vehicle to enter the major road $(\mathrm{s})$

ISD passenger car (left turn from stop) $=0.278 \times 50 \times 7.5=104 \mathrm{~m}$

Table 9.9.5: Time Gap for Case B2—Right Turn from Stop and Case B3—Crossing Maneuver

| Design Vehicle | Time Gap $\left(t_{g}\right)(s)$ at <br> Design Speed of Major Road |
| :--- | :---: |
| Passenger car | 6.5 |
| Single-unit truck | 8.5 |
| Combination truck <br> (WB 19 and WB 20) | 10.5 |

ISD passenger car (right turn from stop) $=0.278 \times 50 \times 6.5=90 \mathrm{~m}$

